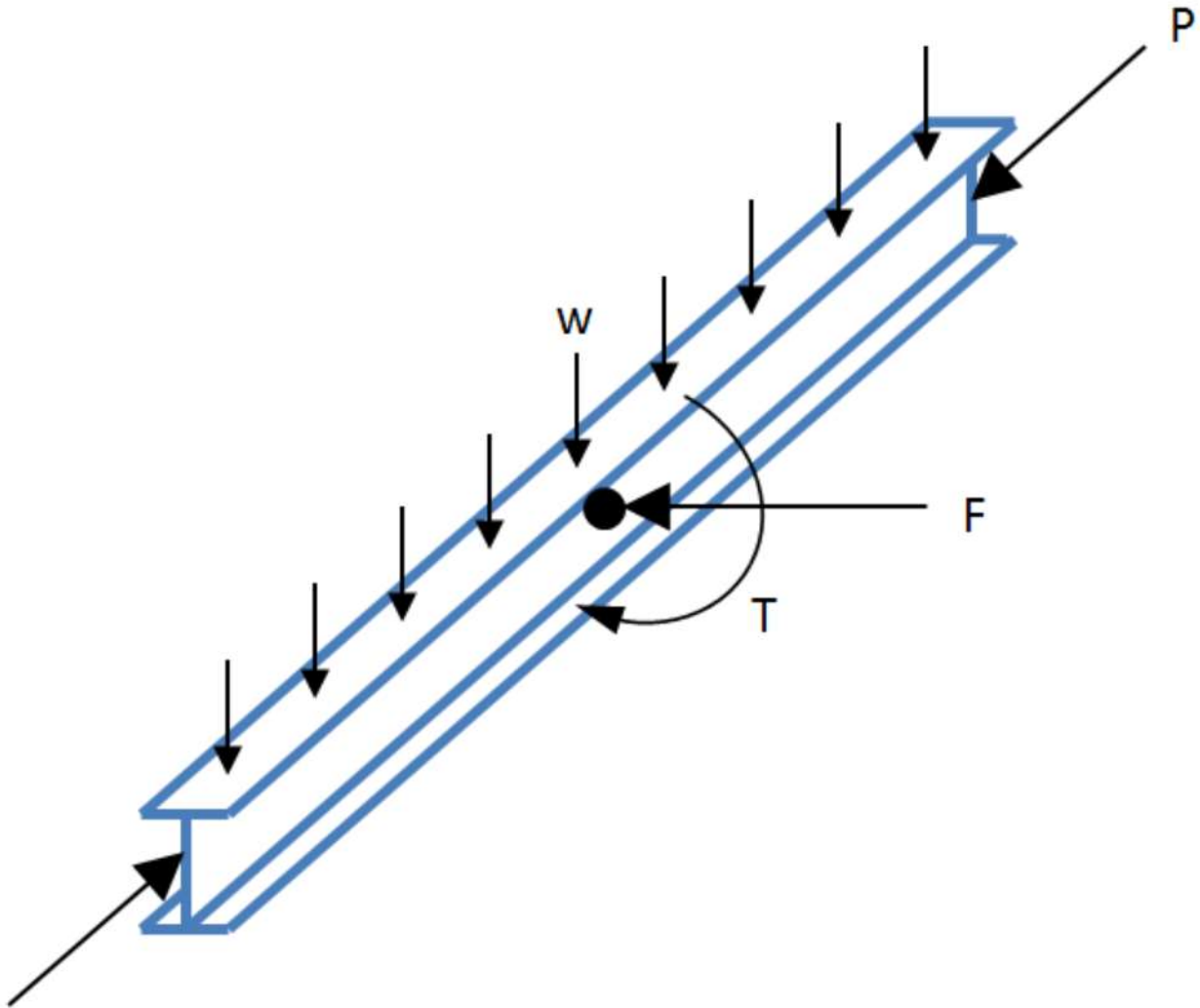


# Simply Supported Beam Design with Torsional Loading

## Using AISC Steel Shapes v14.1 Data

### ▼ Introduction

This application performs a design analysis on a simply supported beam with torsional loading for a W10X54 steel beam (as defined by the AISC Steel Shapes Database). The application follows the design code and equations in AISC 360-10.



References:

- *Simplified Design for Torsional Loading of Rolled Steel Members*, Lin, P.H., Engineering Journal, AISC, 1977
- *2010 Specification for Structural Steel Buildings (ANSI/AISC 360-10)*, Fourth Printing (<https://www.aisc.org/content.aspx?id=2884>)

You will need to install the AISC Shapes Database package from the [MapleCloud](#) before you can use this application.

## ▼ Load the AISC Package

- > `with(AISCShapes) :`
- > `with(Units[Standard]) :`

## ▼ Data from the AISC Shapes Database for Steel Shape W10X54

>  $C_w := \text{Property}(\text{"W10X54"}, \text{"Cw"});$   
 $\text{Property}(\text{"W10X54"}, \text{"Cw"}, \text{"metadata"})$

$$C_w := 2320.0 \text{ in}^6$$

"Warping constant"

(3.1)

>  $J_T := \text{Property}(\text{"W10X54"}, \text{"J"});$   
 $\text{Property}(\text{"W10X54"}, \text{"J"}, \text{"metadata"})$

$$J_T := 1.82 \text{ in}^4$$

"Torsional moment of inertia"

(3.2)

>  $d := \text{Property}(\text{"W10X54"}, \text{"d"});$   
 $\text{Property}(\text{"W10X54"}, \text{"d"}, \text{"metadata"})$

$$d := 10.1 \text{ in}$$

"Overall depth of member, or width of shorter leg for angles, or width of the outstanding legs of long legs back-to-back double angles, or the width of the back-to-back legs of short legs back-to-back double angles" (3.3)

>  $S_x := \text{Property}(\text{"W10X54"}, \text{"Sx"});$   
 $\text{Property}(\text{"W10X54"}, \text{"Sx"}, \text{"metadata"})$

$$S_x := 60.0 \text{ in}^3$$

"Elastic section modulus about the x-axis"

(3.4)

>  $S_y := \text{Property}(\text{"W10X54"}, \text{"Sy"});$   
 $\text{Property}(\text{"W10X54"}, \text{"Sy"}, \text{"metadata"})$

$$S_y := 20.6 \text{ in}^3$$

"Elastic section modulus about the y-axis"

(3.5)

>  $r_x := \text{Property}(\text{"W10X54"}, \text{"rx"});$   
 $\text{Property}(\text{"W10X54"}, \text{"rx"}, \text{"metadata"})$

$$r_x := 4.37 \text{ in}$$

"Radius of gyration about the x-axis =  $\sqrt{I_x/A}$ "

(3.6)

>  $A := \text{Property}(\text{"W10X54"}, \text{"A"});$   
 $\text{Property}(\text{"W10X54"}, \text{"A"}, \text{"metadata"})$

$$A := 15.8 \text{ in}^2$$

"Cross-sectional area of member"

(3.7)

>  $Z_x := \text{Property}(\text{"W10X54"}, \text{"Zx"});$   
 $\text{Property}(\text{"W10X54"}, \text{"Zx"}, \text{"metadata"})$

$$Z_x := 66.6 \text{ in}^3$$

"Plastic section modulus about the x-axis"

(3.8)

>  $I_x := \text{Property}(\text{"W10X54"}, \text{"Ix"});$

`Property("W10X54", "Ix", "metadata")`

$$I_x := 303.0 \text{ in}^4$$

"Moment of inertia about the x-axis"

(3.9)

> `Iy := Property("W10X54", "Iy");`

`Property("W10X54", "Iy", "metadata")`

$$I_y := 103.0 \text{ in}^4$$

"Moment of inertia about the y-axis"

(3.10)

## ▼ Parameters

Gravity distributed load:

>  $w := 1.15 \frac{\text{kipf}}{\text{ft}} :$

Lateral point load at the middle:

>  $F := 5 \text{ kipf} :$

Torsion at mid-span:

>  $T := 5.1 \text{ ft kipf} :$

Axial Load:

>  $P := 96 \text{ kipf} :$

Beam length:

>  $L := 15 \text{ ft} :$

Beam yield stress:

>  $F_y := 50 \text{ ksi} :$

Vertical bending unbraced length:

>  $L_b := 15 \text{ ft} :$

Axial vertical unbraced length:

>  $L_x := 15 \text{ ft} :$

Axial horizontal unbraced length:

>  $L_y := 7.5 \text{ ft} :$

Young's modulus and shear modulus:

>  $E := 29000 \text{ ksi} :$

>  $G := 11200 \text{ksi}$  :

Torsional property (Phillip, 1977):

$$\lambda := \sqrt{\frac{G \cdot J_T}{E \cdot C_w}}$$

$0.01740610961 \frac{1}{\text{in}}$  (4.1)

## ▼ Determine Governing Moments at Middle of Span

Flexural moment:

$$M_x := \frac{wL^2}{8}$$

$32.34 \text{ foot kipf}$  (5.1)

$$M_y := \frac{FL}{4.0}$$

$18.75 \text{ foot kipf}$  (5.2)

$$M_0 := \frac{TL}{4d}$$

$22.72 \text{ foot kipf}$  (5.3)

Philip page 101

$$\beta := \frac{4 \sinh\left(\frac{\lambda L}{2}\right)^2}{\lambda L \sinh(\lambda L)}$$

$\beta := 0.5850278056$  (5.4)

Torsional moment:

$$M_T := \beta M_0$$

$13.29 \text{ foot kipf}$  (5.5)

## ▼ Check Torsional Capacity (AISC 360-10 H3.3 & Philip page 100)

Maximum combined normal stress at the load point:

$$f_{bx} := \frac{M_x}{S_x} + \frac{2 M_T}{S_y}$$

$21.96 \frac{\text{kipf}}{\text{inch}^2}$  (6.1)

Safety factor for compression:

>  $\Omega := 1.67$  :

$$\begin{aligned} > F_{nx} := \frac{F_y}{\Omega} \\ & 29.94 \text{ ksi} \end{aligned} \tag{6.2}$$

$$\begin{aligned} > \frac{f_{bx}}{F_{nx}} \\ & 0.7333393767 \end{aligned} \tag{6.3}$$

This is less than 1, so it is satisfactory.

## ▼ Check Combined Compression and Bending Capacity (AISC 360-10, H1)

$$\begin{aligned} > M_{rx} := \left( \frac{M_x}{S_x} + \frac{2 MT}{S_y} \right) S_x \\ & 109.78 \text{ foot kipf} \end{aligned} \tag{7.1}$$

Effective length factor:

$$> K := 0.85 :$$

Elastic buckling stress:

$$\begin{aligned} > F_e := \frac{\pi^2 E}{\left( \frac{KL}{r_x} \right)^2} \\ & 233.50 \text{ ksi} \end{aligned} \tag{7.2}$$

Critical stress:

$$\begin{aligned} > F_{cr} := 0.658^{\frac{F_y}{F_e}} F_y \\ & 45.71 \text{ ksi} \end{aligned} \tag{7.3}$$

$$> P_n := F_{cr} A$$

$$722.27 \text{ kipf} \tag{7.4}$$

Allowable axial strength:

$$\begin{aligned} > P_c := \frac{P_n}{\Omega} \\ & 432.50 \text{ kipf} \end{aligned} \tag{7.5}$$

This is greater than 3/4 Pr, so it is satisfactory.

Available flexural strength (Chapter F AISC 360-10):

$$\begin{aligned} > M_n := \min(F_y Z_x, F_y S_x) \\ & 250.00 \text{ foot kipf} \end{aligned} \tag{7.6}$$

$$> M_{cx} := \frac{Mn}{\Omega}$$

149.70 foot kipf (7.7)

This is greater than Mrx, so it is satisfactory.

$$> M_{cy} := \frac{Mn}{\Omega}$$

149.70 foot kipf (7.8)

These should be below 1 for a satisfactory design.

$$> \frac{P}{P_c} + \frac{8}{9} \cdot \left( \frac{M_{rx}}{M_{cx}} + \frac{M_y}{M_{cy}} \right)$$

.99 (7.9)

## ▼ Determine Deflections

Max twist angle (Lin, p100 eq4) in degrees:

$$> \phi := \frac{T}{2 G J T \lambda} \cdot \left( \frac{\lambda \cdot L}{2} - \frac{2 \cdot \sinh\left(\frac{\lambda \cdot L}{2}\right)}{\sinh(\lambda \cdot L)} \right) \cdot \sinh\left(\frac{\lambda \cdot L}{2}\right)$$

$\phi := 0.2304416908$  (8.1)

$$> I_3 := I_x \sin\left(\frac{(90 - \phi) \pi}{180}\right)^2 + I_y \cos\left(\frac{(90 - \phi) \pi}{180}\right)^2$$

303.00 in<sup>4</sup> (8.2)

$$> I_4 := I_x \cos\left(\frac{(90 - \phi) \pi}{180}\right)^2 + I_y \sin\left(\frac{(90 - \phi) \pi}{180}\right)^2$$

103.00 in<sup>4</sup> (8.3)

Vertical deflection at the middle:

$$> \Delta_{vert} := \frac{5 w L^4}{384 E I_3}$$

.15 in (8.4)

Horizontal deflection at the middle:

$$> \Delta_{horiz} := \frac{F L^3}{48 E I_4}$$

.20 in (8.5)

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