

Input data:

$$\begin{aligned} > t_6 := 480 \text{ degC}; p_6 := 9 \text{ MPa}; p_7 := 4.76 \text{ kPa} \\ & \quad t_6 := 480 \text{ }^\circ\text{C} \\ & \quad p_6 := 9 \text{ MPa} \\ & \quad p_7 := 4.76 \text{ kPa} \end{aligned} \quad (2.1.1)$$

Specific entropy of fresh (live) steam (the turbine inlet):

$$\begin{aligned} > s_6 := \text{Property}(\text{entropy}, \text{pressure} = p_6, \text{temperature} = t_6, \text{water}) \\ & \quad 6.593 \frac{\text{kJ}}{\text{kg K}} \end{aligned} \quad (2.1.2)$$

Specific enthalpy of fresh (live) steam (the turbine inlet):

$$\begin{aligned} > h_6 := \text{Property}(\text{enthalpy}, \text{pressure} = p_6, \text{temperature} = t_6, \text{water}) \\ & \quad 3,336.4 \frac{\text{kJ}}{\text{kg}} \end{aligned} \quad (2.1.3)$$

Outlet steam specific entropy from the turbine (an ideal process of the steam extension)

$$> s_7 := s_6 :$$

Dryness of steam in outlet of the turbine:

$$\begin{aligned} > x_7 := \text{Property}(Q, P = p_7, \text{entropy} = s_7, \text{water}) \\ & \quad 77.13\% \end{aligned} \quad (2.1.4)$$

Outlet wet steam temperature from the turbine

$$\begin{aligned} > t_7 := \text{Property}(\text{temperature}, \text{pressure} = p_7, Q = 1, \text{water}) : t_7 - 273.15 \text{ K} \\ & \quad 32.0 \text{ }^\circ\text{C} \end{aligned} \quad (2.1.5)$$

Outlet wet steam specific enthalpy from of the turbine:

$$\begin{aligned} > h_7 := \text{Property}(\text{enthalpy}, T = t_7, Q = x_7, \text{water}) \\ & \quad 2,004.4 \frac{\text{kJ}}{\text{kg}} \end{aligned} \quad (2.1.6)$$

Specific work of steam in the turbine:

$$\begin{aligned} > w_{st} := h_6 - h_7 \\ & \quad 1,332.0 \frac{\text{kJ}}{\text{kg}} \end{aligned} \quad (2.1.7)$$

Specific enthalpy of water at saturated line at temperature in the condenser

$$\begin{aligned} > hw_7 := \text{Property}(\text{enthalpy}, T = t_7, Q = 0, \text{water}) \\ & \quad 134.1 \frac{\text{kJ}}{\text{kg}} \end{aligned} \quad (2.1.8)$$

Specific entropy of water at saturated line at temperature in the condenser

$$\begin{aligned} > sw_7 := \text{Property}(\text{entropy}, T = t_7, Q = 0, \text{water}) \\ & \quad .4643 \frac{\text{kJ}}{\text{kg K}} \end{aligned} \quad (2.1.9)$$

Specific enthalpy of condensate

$$> h_8 := hw_7 :$$

Pressure of feed water

$$> p_9 := p_6 :$$

Specific entropy of feed water (an ideal process in the pump):

$$> s_9 := sw_7 :$$

Temperature of feed water:

$$> t_9 := \text{Property}(\text{temperature}, \text{pressure} = p_9, \text{entropy} = s_9, \text{water}) : t_9 - 273.15\text{K} \\ 32.2 \text{ } ^\circ\text{C} \quad (2.1.10)$$

Specific enthalpy of feed water:

$$> h_9 := \text{Property}(\text{enthalpy}, \text{pressure} = p_9, \text{temperature} = t_9, \text{water}) \\ 143.1 \frac{\text{kJ}}{\text{kg}} \quad (2.1.11)$$

Specific useful work of the feed pump:

$$> w_p := h_9 - hw_7 \\ 9.02 \frac{\text{kJ}}{\text{kg}} \quad (2.1.12)$$

Specific heat supplied to the boiler:

$$> q_b := h_6 - h_9 \\ 3193.3 \frac{\text{kJ}}{\text{kg}} \quad (2.1.13)$$

Hence the thermal efficiency of the steam turbine cycle:

$$> \eta_{tst} := \frac{w_{st} - w_p}{q_b} \\ 41.43\% \quad (2.1.14)$$

▼ Gas turbine cycle

Input data:

$$> t_1 := 15\text{degC}; p_1 := 0.1\text{MPa}; p_2 := 1\text{MPa}; t_3 := 1100\text{degC}; t_5 := 130\text{degC} \\ t_1 := 15 \text{ } ^\circ\text{C} \\ p_1 := 0.1 \text{ MPa} \\ p_2 := \text{MPa} \\ t_3 := 1100 \text{ } ^\circ\text{C} \\ t_5 := 130 \text{ } ^\circ\text{C} \quad (2.2.1)$$

Specific enthalpy of fresh air

$$> h_1 := \text{Property}(\text{enthalpy}, \text{pressure} = p_1, \text{temperature} = t_1, \text{air}) \\ 414.38 \frac{\text{kJ}}{\text{kg}} \quad (2.2.2)$$

Specific entropy of fresh air

$$> s_1 := \text{Property}(\text{entropy}, \text{pressure} = p_1, \text{temperature} = t_1, \text{air}) \\ 3.8500 \frac{\text{kJ}}{\text{kg K}} \quad (2.2.3)$$

Outlet air specific entropy, temperature and specific enthalpy from the compressor

$$> s_2 := s_1 : \\ > t_2 := \text{Property}(\text{temperature}, \text{pressure} = p_2, \text{entropy} = s_2, \text{air}) : t_2 - 273.15\text{K} \\ 279.46 \text{ } ^\circ\text{C} \quad (2.2.4)$$

$$> h_2 := \text{Property}(\text{enthalpy}, \text{pressure} = p_2, \text{temperature} = t_2, \text{air})$$

$$683.60 \frac{\text{kJ}}{\text{kg}} \quad (2.2.5)$$

Inlet gas pressure, specific entropy and specific enthalpy to the gas turbine

$$> p_3 := p_2 :$$

$$> s_3 := \text{Property}(\text{entropy, pressure} = p_3, \text{temperature} = t_3, \text{air})$$

$$4.867 \frac{\text{kJ}}{\text{kg K}} \quad (2.2.6)$$

$$> h_3 := \text{Property}(\text{enthalpy, pressure} = p_3, \text{temperature} = t_3, \text{air})$$

$$1,610.34 \frac{\text{kJ}}{\text{kg}} \quad (2.2.7)$$

Outlet gas pressure, specific entropy, temperature and specific enthalpy from the gas turbine

$$> p_4 := p_1 :$$

$$> s_4 := s_3 :$$

$$> t_4 := \text{Property}(\text{temperature, pressure} = p_4, \text{entropy} = s_4, \text{air}) : t_4 - 273.15\text{K}$$

$$498.01 \text{ } ^\circ\text{C} \quad (2.2.8)$$

$$> h_4 := \text{Property}(\text{enthalpy, pressure} = p_4, \text{temperature} = t_4, \text{air})$$

$$916.82 \frac{\text{kJ}}{\text{kg}} \quad (2.2.9)$$

Specific heat supplied to the combustion chamber:

$$> q_1 := h_3 - h_2$$

$$926.74 \frac{\text{kJ}}{\text{kg}} \quad (2.2.10)$$

Specific work of the gas turbine

$$> w_{gt} := h_3 - h_4$$

$$693.52 \frac{\text{kJ}}{\text{kg}} \quad (2.2.11)$$

Specific work of the air compressor

$$> w_c := h_2 - h_1$$

$$269.23 \frac{\text{kJ}}{\text{kg}} \quad (2.2.12)$$

Hence the thermal efficiency of the gas turbine cycle:

$$> \eta_{tgt} := \frac{w_{gt} - w_c}{q_1}$$

$$45.78\% \quad (2.2.13)$$

▼ Combined (binary) cycle

Outlet gas pressure and specific enthalpy from the steam boiler

$$> p_5 := p_4 :$$

$$> h_5 := \text{Property}(\text{enthalpy, pressure} = p_5, \text{temperature} = t_5, \text{air})$$

$$530.5 \frac{\text{kJ}}{\text{kg}} \quad (2.3.1)$$

Ratio of gas and steam mass flow

$$\begin{aligned} > m := \frac{h_6 - h_9}{h_4 - h_5} \\ & \qquad \qquad \qquad 8.265 \qquad \qquad \qquad (2.3.2) \end{aligned}$$

Specific heat supplied to the combustion chamber:

$$\begin{aligned} > q_1 := m \cdot (h_3 - h_2) \\ & \qquad \qquad \qquad 7659.4 \frac{\text{kJ}}{\text{kg}} \qquad \qquad \qquad (2.3.3) \end{aligned}$$

Specific work of the gas turbine cycle

$$\begin{aligned} > w_{gtc} := (h_3 - h_4) - (h_2 - h_1) \\ & \qquad \qquad \qquad 424.3 \frac{\text{kJ}}{\text{kg}} \qquad \qquad \qquad (2.3.4) \end{aligned}$$

Specific work of the steam turbine cycle

$$\begin{aligned} > w_{stc} := (h_6 - h_7) - (h_9 - h_8) \\ & \qquad \qquad \qquad 1323.0 \frac{\text{kJ}}{\text{kg}} \qquad \qquad \qquad (2.3.5) \end{aligned}$$

Hence the thermal efficiency of the Combined (binary) cycle is higher than separate steam or gas turbine cycles:

$$\begin{aligned} > \eta_{tbc} := \frac{m \cdot w_{gtc} + w_{stc}}{q_1} \\ & \qquad \qquad \qquad 63.06\% \qquad \qquad \qquad (2.3.6) \\ > \end{aligned}$$